
ATW Simulations and the Role of Nuclear Cross-Section Data

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Assumptions for Current ATW Design

- **Cylindrical lead-bismuth-eutectic (LBE) target (18 to 25 cm in radius) with proton beam entering from top**
- **Hexagonal/cylindrical blanket surrounds target (radius ~100 cm)**
- **Blanket consists of actinide/zirconium fuel rods with stainless-steel (SS) cladding and LBE coolant (this may be changed to sodium)**
- **ATW fuel is plutonium and minor actinides plus 0.005% residual uranium in transuranic (TRU) fuel from light-water-reactor(LWR) spent fuel**



Neutronics Issues

- As material is burned, so are fissile isotopes, and the effective multiplication factor (k_{eff}) drops
- To maintain chain reaction/power, $(1 - k_{\text{eff}})$ fraction of neutrons must be produced by accelerator – higher (~ 0.95 to 0.97) and more stable k_{eff} preferred
- The harder (faster) the spectrum, the higher the actinide fission-to-capture ratio, which allows more effective transmutation
- Once the system is started, fission products and uranium are removed each cycle (4-6 months) and new actinides added until an equivalent amount of each actinide added is burned (steady state)



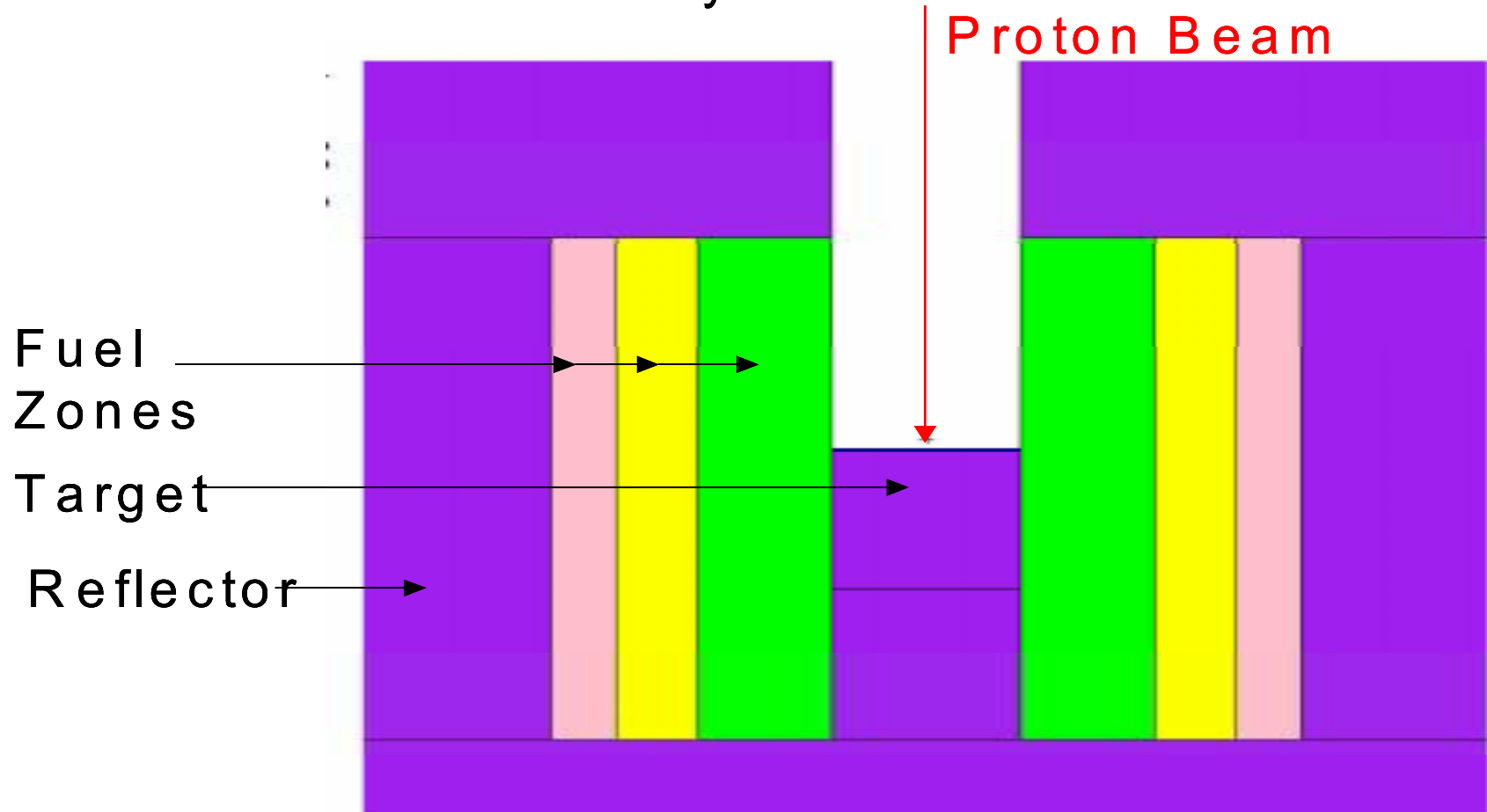
Sample Composition of ATW Fuel

| Isotope | Average Core Composition |
|---------|--------------------------|
| U-238 | 0.17 |
| Np-237 | 3.36 |
| Pu-238 | 5.95 |
| Pu-239 | 27.29 |
| Pu-240 | 35.68 |
| Pu-241 | 5.46 |
| Pu-242 | 10.12 |
| Am-241 | 6.15 |
| Am-242m | 0.54 |
| Am-243 | 1.90 |
| Cm-242 | 0.43 |
| Cm-243 | 0.03 |
| Cm-244 | 2.15 |



Cross-Sectional View of LBE Target/Blanket Configuration

Profile of ATW LBE System



Cross-Section Studies

• Isotopes Examined

- Pu-238
- Pu-239
- Pu-240
- Pu-241
- Pu-242
- Np-237
- Am-241
- Cm-242
- Cm-244

For each MCNP run, the library of one isotope was changed, with ENDF-VI libraries being the default

• Libraries

- JEF-2
- JENDL-3.2
- BROND-2
- CENDL-2



Parameters Examined

- k_{eff} and assoc. error
- Delayed Neutron Fraction (β)
- ν number of neutrons generated per fission
- Capture and Fission Cross Sections
- Fission-to-Capture Ratio
- Void Reactivity Coefficient (0 and 10% coolant)
- Temperature Reactivity Coefficient (980K – 1580K)
- Remember: Statistics DO affect results!!!
(this contributes to large changes in void react. coeff. and positive temp. react. coeff.)



Basecase Parameters

- $k_{\text{eff}} = 0.95726$
- $\beta = 0.00418$ = one \$ in further reactivity calculations
- $\nu = 3.01$
- $\sigma_c = 0.117$ barns
- $\sigma_f = 0.145$ barns
- Temperature Reactivity Coeff = $-\$0.18$
- Void Reactivity Coeff = $-\$75$
- 10% Coolant Reactivity Coeff = $-\$63.5$



Pu-239

| measure | JEF | JENDL | BROND | CENDL |
|-----------|---------|---------|---------|---------|
| keff | 0.95037 | 0.957 | 0.95117 | 0.9573 |
| error | 0.00165 | 0.0018 | 0.00194 | 0.00199 |
| capt. xs | 0.12481 | 0.12461 | 0.12677 | 0.1233 |
| fiss. xs | 0.16964 | 0.16868 | 0.16862 | 0.16985 |
| fiss/capt | 1.35927 | 1.35364 | 1.33014 | 1.37757 |
| nu | 3.00617 | 3.00915 | 3.00148 | 3.0032 |

Pu-240

| measure | JEF | JENDL | BROND | CENDL |
|-----------|---------|---------|---------|---------|
| keff | 0.9504 | 0.95035 | 0.96168 | 0.95388 |
| error | 0.00185 | 0.00167 | 0.00155 | 0.0016 |
| capt. xs | 0.12763 | 0.12759 | 0.12729 | 0.12487 |
| fiss. xs | 0.16868 | 0.16782 | 0.16899 | 0.16824 |
| fiss/capt | 1.32159 | 1.31529 | 1.32762 | 1.34726 |
| nu | 3.00227 | 3.00506 | 3.02187 | 3.0069 |

Np-237

| measure | JEF | JENDL | CENDL |
|-----------|---------|---------|---------|
| keff | 0.95593 | 0.95771 | 0.95489 |
| error | 0.00184 | 0.00188 | 0.00186 |
| capt. xs | 0.12489 | 0.12456 | 0.12392 |
| fiss. xs | 0.16898 | 0.16905 | 0.16889 |
| fiss/capt | 1.3531 | 1.35722 | 1.36298 |
| nu | 3.01574 | 3.0094 | 3.00781 |

Am-241

| measure | JEF | JENDL | CENDL |
|-----------|---------|---------|---------|
| keff | 0.95626 | 0.95531 | 0.95798 |
| error | 0.00181 | 0.00184 | 0.00228 |
| capt. xs | 0.12561 | 0.12207 | 0.1244 |
| fiss. xs | 0.16881 | 0.16878 | 0.16896 |
| fiss/capt | 1.34395 | 1.38261 | 1.35825 |
| nu | 3.00767 | 3.0044 | 3.00713 |

Cm-242

| measure | JEF | JENDL | BROND |
|-----------|---------|---------|---------|
| keff | 0.95699 | 0.95791 | 0.95257 |
| error | 0.00166 | 0.00211 | 0.00168 |
| capt. xs | 0.12487 | 0.12516 | 0.12406 |
| fiss. xs | 0.16948 | 0.1694 | 0.16929 |
| fiss/capt | 1.35727 | 1.35349 | 1.36454 |
| nu | 3.01205 | 3.01078 | 3.00932 |

Cm-244

| measure | JEF | JENDL | BROND |
|-----------|---------|---------|---------|
| keff | 0.95494 | 0.95836 | 0.95639 |
| error | 0.00164 | 0.00183 | 0.00184 |
| capt. xs | 0.12397 | 0.12368 | 0.12352 |
| fiss. xs | 0.16894 | 0.169 | 0.16883 |
| fiss/capt | 1.36278 | 1.36641 | 1.3668 |
| nu | 3.00381 | 2.99994 | 3.02053 |

Pu-238

| measure | JEF | JENDL | BROND |
|-----------|---------|---------|---------|
| keff | 0.9564 | 0.95914 | 0.95947 |
| error | 0.00169 | 0.00174 | 0.00166 |
| capt. xs | 0.12284 | 0.12322 | 0.12247 |
| fiss. xs | 0.16919 | 0.169 | 0.16877 |
| fiss/capt | 1.37732 | 1.37152 | 1.37801 |
| nu | 3.00717 | 3.00078 | 2.996 |

Pu-241

| measure | JEF | JENDL | BROND |
|-----------|---------|---------|---------|
| keff | 0.95531 | 0.95252 | 0.95703 |
| error | 0.00179 | 0.00158 | 0.00186 |
| capt. xs | 0.12593 | 0.12493 | 0.12407 |
| fiss. xs | 0.16886 | 0.16893 | 0.16876 |
| fiss/capt | 1.34088 | 1.35216 | 1.36019 |
| nu | 3.00828 | 3.00385 | 3.01076 |

Pu-242

| measure | JEF | JENDL | BROND |
|-----------|---------|---------|---------|
| keff | 0.95366 | 0.94999 | 1.03128 |
| error | 0.00173 | 0.00178 | 0.00202 |
| capt. xs | 0.12507 | 0.12443 | 0.11645 |
| fiss. xs | 0.16904 | 0.16852 | 0.19241 |
| fiss/capt | 1.35163 | 1.35435 | 1.65222 |
| nu | 3.00299 | 3.0102 | 2.97714 |

Conclusions

- **Variances are seen by using different libraries**
- **Cross-section libraries had largest effects on most abundant isotopes (Pu-240 is best example)**
- **Pu-242's BROND library showed greatest deviation in k_{eff}**
- **Better accuracy is needed to reduce statistical effects**

